The Sound Strobe

With this simple diagnostic tool, you can test the sound of

your loudspeakers. . . without hauling them to the lab.

By Dennis Colin

istening to these pulse signals, with six selectable spectrum shapes, is very revealing of loudspeaker time smear (driver "hangover," crossover misalignment, cabinet diffraction, and so on), frequency response colorations (particularly from resonances), and room effects such as discrete echoes, standing-wave bass modes, and acoustic colorations in general. You can hear quickly, and with detailed clarity, the speaker's degree of image focus, transient precision, and tonal neutrality.

OVERVIEW

Six pulse shapes are generated with a pulse repetition frequency (PRF) of 0.5-41.2Hz (see unit in Photos 1-4). The lower (rhythmic) rates allow hearing detailed decay patterns, while the audio rates (41.2Hz is the low "E" on a 4-string bass) provide harmonicallyrich tones very sensitive to response and coherence anomalies. The selectable spectral distributions range from linear to non-resonantly shaped, allowing a focus on various frequency ranges. The impulse waveform and a linear ramp sawtooth are also provided at additional outputs, useful for oscilloscope triggering and X-Y plots.

The compact $(8^{1}4'' \times 5^{3}4'' \times 3^{3}2')$ low cost generator is powered by two rechargeable 9V batteries or an AC line "wall wart" (**Photos 5** and **6**); the batteries will power the unit for about 10 hours/charge.

APPLICATIONS

Listening to test signals is, of course, no substitute for music evaluation. Rather, these wideband coherent-transient pulses serve as an auditory diagnostic tool; repeatable signals allow sonic identification of a wide variety of speaker and room anomalies. The time-coherent nature of the pulses allows you to simultaneously hear and distinguish both the direct speaker output's image focus and a plethora of room effects. Walking around the room, you can identify reflective surfaces contributing colorations, discrete echoes, and so on.

An additional application is peak power testing for distortion and com-

pression: with the short-duration $(14.5\mu s)$ impulse waveform, you can even test a tweeter at 1kW peak, because even at the maximum PRF of 41.2Hz the average power is only 0.5W.

WAVEFORM DATA

Figure 1 shows the six waveforms, spectral distributions, pulse widths, and RMS to peak voltage ratios at two PRFs, 5Hz, and 40Hz. Squaring these





WAVEFORM (NOTE DIFFERENT TIME SCALES)	20 SPECTRUM 20 Hz (PER OCT. BASIS) ↓	SLOPES AB/OCT	РULSE WIDTH @ 50% Vpk	VRMS VPK PRF=40Hz	VRMS VPK PRF=5H
1MPULSE 100/8/div		+3	5ىر 14.5	0.022	0.008
"PINK PULSE" 100/5/div	· · · · · · · · · · · · · · · · · · ·	0	2 م 20	0.033	0.012
EXP ³ L PULSE TC=252µS Im5/div	632. Hz	+3,-3	5 م 5 7 1	0.075	0.026
EXP'L PULSE TC=830yS ImS/div	192 Hz	+3, -3	575 × S	0.122	0.043
EXP ² L pulse TC=25m5 Iom5/div		-3	17.5 m S	0.493	0.248
LOW FREQ. PULSE SmS/div	2.00 Hz	0,-15	3•8m5	0+342	0-128

SPECIAL SPEAKER SECTION

ratios gives the ratios of average to peak power delivered to the speaker, useful for ensuring safe high-peak-power testing for compression and distortion. Figure 2 shows an example of this high power testing. The impulse signal was amplified by "Mad Katy" (Photo 7), a 125W per channel stereo tube amp I designed. Driven to just below clipping in bridged monoblock mode, a peak impulse power of 450W was delivered to a Swans M1 speaker (average impedance about 8Ω). This excellent mini-monitor with ribbon tweeter (which I reviewed in SB 3/99) had no problem handling the 450W peak impulse, as shown by the very small change regarding the response with 18W peak power.

The 450W peak impulse, at the 20Hz PRF I used, produced an average power of only 0.11W. Perceived loudness was closer to the 113dB peak SPL than the 77dB average SPL. The sound was very "snappy," similar to that of electric sparks. It was very easy to distinguish the direct speaker output (crisp "snaps" with almost no tonal color) from the room sound (an enveloping "ocean" of thousands of pulse harmonics with tonality sustained by standing waves, and discrete pulse reflections originating from localizable reflecting surfaces).

When I moved about the room, the reverberation became a massive 3D "chorus effect" of moving pulses and

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changing overtone patterns, yet the speaker's directly-radiated impulses maintained the precise focus and tonal neutrality that I praised the Swans M1 for in the review.

The spectrum of a single impulse (for practical purposes, a unipolar pulse of shorter duration than a quarter cycle of the highest frequency of interest) is continuous and flat, with constant bandwidth (BW) analysis; that is, there's equal power per Hz BW across the band.

However, the ear analyzes on a frequency-proportional basis; that is, power per octave (or fraction thereof). Therefore, a flat *per-Hz* spectrum signal, such as an impulse or white noise, is perceived as having a 3dB/octave upward slope; that's why white noise sounds thin and "hissy." Conversely, pink noise sounds flat, spectrally balanced; its spectrum slopes downward (-3dB/octave) on a per-Hz analysis, but is flat on a per-octave basis. The spectra in **Fig. 1** are with per-octave analysis, the way we hear.

SPECIFIC WAVEFORM DESCRIPTIONS

1. Impulse

Figure 3 shows this on an expanded $(5\mu s/div)$ time scale; pulse width at 50% Vpeak is 14.5 μ s; 10-90% rise and fall times are about 6 μ s. Compared with an ideal impulse, the spectrum is -1dB at 20kHz, and -3dB at 30kHz.

FIGURE 2: High power impulse testing of speaker.



The sound (on a very neutral and coherent speaker) is very "snappy" and colorless like a small electric spark, but not as "sizzly bright"—that's because a small (<¼") spark radiates an acoustic doublet waveform: a differentiated impulse with spectrum sloped up 6dB/octave with reference to an impulse. (Lightning, a very

- 5uS

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SB-2581-03

SPECIAL SPEAKER SECTION

big spark, radiates nearly a step function sound wave, with bass to below 1Hz.)

The impulse, with its linear upwardsloping spectrum (to the ear), is best for hearing tweeter reflections, diffraction, and other anomalies of time coherence and HF tonal neutrality.

2. "Pink Pulse"

Figure 4 shows this on a range of



time scales. This waveform has several interesting properties:

- a) A flat spectrum on a per-octave basis (as the ear analyzes), like pink noise (hence the name).
- b) The decay looks similar over a wide range of time scales.

FIGURE 5: LF pulse at 41.2Hz PRF.



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3-chambe BP prism c) An ideal pink pulse (infinite BW) would initiate with a jump to infinity, and decay inversely proportional to the square root of time. The pulse shown has a -3dB rolloff at 30kHz.
d) With constant BW (e.g., per Hz) spectral analysis, such as is used in Laplace transforms, the (ideal) pink pulse is the only non-repeating waveform whose shape is identical to that of its spectrum: the spectral amplitude is proportional to 1/√frequency; that is, a slope of -3dB/octave with constant BW analysis (flat to the ear).

The sound has a sharp attack like the impulse, but has "full-bodied" midrange and bass, rather than the predominant HF "snap." It's basically a tonally-neutral full-band precision "click," extremely revealing of time and tonal response anomalies across the audio spectrum. Only with the very best speakers will this pulse maintain its pristine transient impact and lack of tonality.

3. Exponential pulse, $252\mu s$ time constant (TC)

As the sonically-perceived spectrum

in **Fig. 1** shows, this pulse has a broad (non-resonant) peak at 632Hz, the logarithmic center of the audio band. This pulse doesn't sound "colored," but the midrange emphasis serves to best reveal midrange response anomalies, while maintaining enough perspective of lower and higher frequencies. The sound (on a good speaker, of course) could be described as a "fat click."

4. Exponential pulse, 830µs TC

This is similar to the previous pulse, but with the non-resonant peak at 192Hz. It's generated by 1st-order highpass filtering a step pulse, rolling it off below 192Hz (-3dB point). It's useful for hearing the step response of small speakers, without subjecting them to the excessive bass power of an unfiltered step pulse. It's also useful for evaluating mid-bass coherence and neutrality.

5. Exponential pulse, 25ms TC

This is basically a raw step pulse, the 25ms TC decay being the result of a 6Hz 1st-order LF rolloff. It's useful for

evaluating full-band coherence and bass impact of large speakers. Caution: it's tempting to turn up the volume enough to feel the impact, rattle the walls, and so on, but with a high-powered amp, woofer damage is quite possible.

6. Low frequency pulse

As the spectrum in **Fig. 1** shows, this pulse doesn't have the rising deep bass energy of the previous pulse, but it's strongly filtered above 200Hz. The sound could be described as a nonresonant "thump," but sharper in precision than that word implies. The spectrum (again, to the ear) is flat from about 20-100Hz. This pulse is useful for hearing bass clarity, impact precision, and tonal neutrality.

Figure 5 shows the waveform and harmonic spectrum when this pulse is repeated at an audio rate, 41.2Hz (the low "E" on a 4-string bass). The rich but smoothly rolled-off harmonic content produces a pleasing, string-like bass tone that serves as a repeatable test of bass coherence and neutrality.



SPECIAL SPEAKER SECTION

OSCILLATOR

U1A (latching comparator or "hysteretic switch") and U1B (integrator) form a

linear-ramp sawtooth oscillator (**Fig. 6a**). Without D1 and R10, the output at U1B pin 7 would be a symmetri-



PHOTO 4a, b: Inside top panel.



PHOTO 5: Battery power supply.





cal triangle wave. But D1 conducts when U1A pin 1 is positive, producing a rapid fall time $(13\mu s)$ at pin 7. Pot R32, R9, R11, and C1 determine the ramp charging time, and therefore the oscillator frequency.

The voltage at pin 1 pulses positive for about 13µs, and stays negative for the rest of the cycle. This waveform, through D2, R26, R27, and C16, produces the impulse signal selectable by S2. The pin 1 pulse also drives the circuitry from D3 to Q1, Q2, which flashes the green LED 1 (140mA for about 100µs, 1mA maximum average DC) in sync with the output pulses.

PINK PULSE Shaper

The ramp reset step from U1 pin 7 has the step function's -6dB/ octave spectrum with constant BW analysis, but -3dB/ octave slope to the

PHOTO 7: "Mad Katy" amp used for impulse power test.



ear. So this is equalized with a +3dB/ octave slope to achieve the desired flat auditory spectrum. Note: the impulse waveform could have been used with a -3dB/octave EQ, but for the same peak voltage limit, the impulse has much less energy.

R4 through R8 and C2 through C5 comprise a -3dB/octave impedance network, accurate within ±0.5dB from 10Hz–25kHz. Connected between the sawtooth step and the output op amp U2B inverting input pin 6 (when selector S2 is in position 5), the network's -3dB/octave impedance/frequency slope adds an upward +3dB/octave slope at the out-





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put (U2 pin 7). Figure 7 shows the 1 kHz square wave (from an external generator) response of the shaping circuit.

EXPONENTIAL PULSES

C6, 7, and 8, with R14, 15, form firstorder high-pass filters, determining the exponential decay time constants. While with constant BW analysis such pulses have a flat spectrum up to the HP filter corner frequency, then slope-down (-6dB/octave), to the ear the spectrum peaks at this frequency as shown in **Fig. 1**.

LF PULSE

The sawtooth wave is first sloped upward (+3dB/octave) by C9, 10 and R19, 20, 21,

to produce a flat auditory spectrum; then it's low-pass-filtered above 200Hz by R22, 23, C11, 12, and C13, R18. The net LP filtered spectrum has a slope of about -15dB/ octave. Consisting of cascaded first (and half)-order networks, the rolloff is nonresonant (sonically uncolored).

Note that in Fig. 5 (harmonic spectrum of LF pulse at a PRF of 41.2Hz),

FIGURE 6a: Sound Strobe schematic.



FIGURE 6b: Schematic of battery charger and power supply.



PARTS LIST

the first few har-

monics decrease

in amplitude by about 3dB/octave,

while the single-

pulse spectrum in

Fig. 1 is flat below

200Hz. This is

because discrete

spectral lines'

amplitudes aren't

subject to analysis

bandwidth, unlike

a spectral contin-

uum such as noise

or single events.

But there's no

contradiction: the

harmonics (below

the 200Hz filter-

ing) do roll off at

about 3dB/octave,

but as frequency

doubles, the num-

ber of harmonics

per octave doubles,

increasing the

power per octave

by a slope of 3dB/

octave. So the net

power/octave that

the ear analyzes

is approximately

constant (below

the 200Hz LP fil-

tering).

SELECTOR

SWITCH S2

In positions 1

through 5 (all

waveforms except

impulse), the out-

put op amp's non-

inverting input is

grounded by S2B,

and the negative-

going sawtooth

step's shaped puls-

es are inverted for

a positive-going

output from U2B.

(impulse output),

the impulse is

fed to U2B non-

inverting input,

while S2A opens

In S2 position 6

Reference Value Description Manufacturer R1 52K3 1%, ¼W, metal film Mouser 271-52.3K Mouser 271-1.74K R2 1740 1%, ¼W, metal film R3 2490 1% ¼W metal film Mouser 271-2.49K R4, R23 Mouser 271-180K 18NK 1%, 1/4W, metal film **R5** 39K2 1%, ¼W, metal film Mouser 271-39.2K 1%, ¼W, metal film Mouser 271-12K **R6** 12K Mouser 271-3.3K 1%, ¼W, metal film **R7** 3300 1%, ¼W, metal film Mouser 271-1.2K **R8** 1200 Mouser 271-2.2M R9 2M2 1%, 1/4W, metal film R10 820 1% ¼W metal film Mouser 271-820 R11 806 1%, 1/4W, metal film Mouser 271-806 1%, 1/4W, metal film Mouser 271-51.1K R12 51K1 1%, ¼W, metal film Mouser 271-150K R13 150K Mouser 271-2.8K R14 2800 1%, ¼W, metal film R15 24K9 1% ¼W metal film Mouser 271-24.9K R16 2000 1%, 1/4W, metal film Mouser 271-2K 1%, ¼W, metal film R17, R21 Mouser 271-10K 10K 56K 1%, ¼W, metal film Mouser 271-56K R18 1%, ¼W, metal film Mouser 271-120K R 19 120K R20, R22 33K 1%, ¼W, metal film Mouser 271-33K R24 1910 1%, ¼W, metal film Mouser 271-1.91K R25 100 1% ¼W metal film Mouser 271-100 R26 560 1%, 1/4W, metal film Mouser 271-560 1500 1%, ¼W, metal film Mouser 271-1.5K R27 R28 100K 1%, ¼W, metal film Mouser 271-100K R29 1000 1%, ¼W, metal film Mouser 271-1K R30 270 1%, ¼W, metal film Mouser 271-270 R31 470 1%, 1/4W, metal film Mouser 271-470 100K Mouser (Alpha) 31VJ501 R32 Pot, audio taper R33 5000 Pot, audio taper Mouser (Alpha) 31VJ305 R34, R35 680 Mouser 273-680 1%, ½W, metal film R36 2000 1%, 1/2W, metal film Mouser 273-2K R37, R38 1%, ¼W, metal film Mouser 271-470 470 R39 604 1%, ½W, metal film Mouser 273-604 C1, C11 15nF 5%, 50V, polyester film Digi-Key (Panasonic) P4584 C2, C6, C9, C23, Digi-Key (Panasonic) P4525 C24, C25, C26 100nF 5%, 50V, polyester film C3, C10 Digi-Key (Panasonic) P4569 33nF 5%, 50 V, polyester film C4 10nF 5%, 50V, polyester film Digi-Key (Panasonic) P4582 C5 3n3 5%, 50V, polyester film Digi-Key (Panasonic) P4557 5%, 50V, polyester film Digi-Key (Panasonic) P4549 C7 330nF C8 10µF 10%, 100V, polyester film Digi-Key (Panasonic) EF1106 C12 2n7 5%, 50V, polyester film Digi-Key (Panasonic) P4556 Digi-Key (Panasonic) P4561 5%, 50V, polyester film C 13 6n8 C14 1n5 5%, 50V, polyester film Digi-Key (Panasonic) P4553 C15, C16 5%, 50V, polyester film Digi-Key (Panasonic) P4551 1nF C17 4n7 5%, 50V, polyester film Digi-Key (Panasonic) P4559 Mouser (Xicon) 140-XRL25V47 47µF 25V, radial electrolytic C 18 C19, C20 100µF 25V, radial electrolytic Mouser (Xicon) 140-XRL25V100 Mouser (Xicon) 140-XRL25V1000 C21, C22 1000µF 25V, radial electrolytic U1, U2 TL082 Dual opamp, 8-pin DIP Mouser (TI) 595-TL082ACP U3 78L06A +6V regulator, TO-92 Digi-Key (Panasonic) AN78L06 79L06A -6V regulator, TO-92 Digi-Key (Panasonic) AN79L06 114 D1, D2, D3, D4, D5 Silicon diode Mouser 1N4148MSCT 1N4148 Mouser 1N4003MSCT 1N4003 D6 Silicon diode LED1 Yellow LED Charge-on indicator Lumax SSI-LXR1612YD (Digi-Key 67-1149) LED2 Green LED Freq indicator Lumax SSI-LXR1612GD (Digi-Key 67-1148) LED3 Red LED Low-battery indicator Lumax SSI-LXR1612ID (DigiKey 67-1147) J1, J3, J4 DGS (Mouser 161-1052) Female, panel mount RCA, black J2 Female, panel mount RCA, red DGS (Mouser 161-1053) J5 2.5mm male, insulated, panel mount, DGS (Mouser 163-4303) power input connector P1, P4, P5, P8 3-pin shell with terminal pins Molex WM2012 P2, P6, P7, Molex WM2011 P9A, P9B, P11 2-pin shell with terminal pins Molex WM2018 P3 9-pin shell with terminal pins 6-pin shell with terminal pins P10 Molex WM2015 (39) terminal pins for the Molex shells Molex WM2200 H1, H4, H5, H8 3-pin male header Molex WM4001 (continues \rightarrow)

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the inverting input. Thus, U2B acts as a voltage follower for the (positive) impulse waveform.

C14 and C15 serve to attenuate ultrasonic pulse components (extending to above 100kHz).

POWER SUPPLY (FIG. 6b)

S1 selects "AC," "off," or "BAT." The suppy selected is regulated to ±6V by U3, U4, and so on. Batteries B1, B2 (9V NiCd) are charged with a tapered current averaging 10mA.

LED1 (yellow) indicates AC power.

LED3 (red), labled "Pwr on," indicates both that and sufficient charge of batteries is used. Note the connection of LED3 differentially across regulator U3, biased by R39 to glow only with sufficient positive battery charge; and because the positive battery (B1) has a slightly higher discharge rate than the negative one (B2)—about 12mA versus 10mA—than LED3 indicates satisfactory charge of both batteries.

Note that the current through LED3 contributes to the positive load current; therefore it is "free." Also, its bright-



PARTS LIST (cont.)

H2, H6, H7, H11	2-pin male header	Molex WM4000	
H3	9-pin male header	Molex WM4007	
H9	4-pin male header	Molex WM4002	
H10	6-pin male header	Molex WM4004	
	(Headers, s from Mou	hells and terminal pins are available ser, Digi-Key, and others.)	
S1	DPDT miniature toggle switch	Digi-Key (Carling) 432-1149	
S2	Rotary switch, 2-pole, 6-positions,		
	break-before-make	Mouser (Lorin) 105-14572	
	Enclosure, 8 × 5 × 3″	Sescom MC-6A	
	Circuit board		
	Front panel	Metalphoto of Cincinnati	
	Stick-on label for rear panel	TDL M121R	
	(3) knobs	Mouser (Eagle Plastics) 45KN017	
	Panel mount 5mm fuse holder	Mouser (Littlefuse) 576-03455LS1H	
	5mm fuse, 0.25A	Digi-Key (Wickmann) WK1035	
	(2) battery holders	Mouser (Keystone) 534-1295	
	(2) battery retaining clips	TDL M401BRC	
	(4) aluminum pop rivets, 1/8" dia × 1/8" grip (to attach battery holders to rear panel)		
	(2) 4-40 × 5/16" machine screws	Mouser H343	
(4) $4-40 \times 5/8''$ machine screws		Mouser H348	
(2) #4 lock washers		Mouser H236	
(6) 4-40 hex nuts		Mouser H216	
	(4) 3/8″ long nylon spacers, tapped 4-40	Mouser (Eagle Plastics) 561-L4.375	
	(4) Stick-on plastic feet for enclosure bottom	Mouser (3M) 517-SJ-5023BK	
	(13') #24 AWG stranded wire		
	(2) 9V rechargeable NiCd batteries	JDR NB9V or equal	
	Wall DC power supply, 24V DC at 100mA	Mouser 412-124013	

Also, its brightness varies with charge level, serving as a "fuel gauge."

USING THE SOUND STROBE

The pulses provided can be very revealing of transient and tonal reproduction characteristics, but first you must know what the pulses should sound like. The short answer is "as sharp, spatially focused, and non-tonal (uncolored) as possible." Think of hearing an electric sparkthere's no tonality, but an immediate "Snap!" that you can locate to within inches from across the room. It's so precisely focused that you instinctively jump to look for it. The best full-

range speakers, electrostatics, planar magnetics, or small cones, can come close to this precision. Many multi-way speakers fall short, and the Sound Strobe pulses are heard spread out in time and space. Admittedly this is unfair; we listen to music, not electronic pulses (except for synthesizers); and (at least acoustic) music doesn't have transients nearly as sharp as electronic impulses. But if you aren't completely satisfied with your speakers (present or contemplated), then these test pulses can help you diagnose and improve their sonic fidelity.

The longer answer to knowing what to listen for is this: I strongly recommend playing all six pulses on the very best speakers available, from friends, willing retailers, and so on. I also recommend good headphones, with their excellent time coherence. Of course, their lack of room acoustics makes for an unfair comparison with speakers; however, the pulses' sharp transient nature, coupled with the Haas (precedence) effect, allows you to distinguish a speaker's direct output from the room reverberation.

It's also informative to listen to the pulses on a wide variety of speakers, from the best to the worst available. Correlating the pulse sound with music will then build up an "experience base" of various transient, focus, and tonal anomalies. Then you can use the repeatable high-resolution pulses to quickly identify problem areas by direct listening (unlike trying to interpret electronic measurements), and without the immense variability of musical sounds.

Of course, the goal is to reproduce this musical variety with the utmost clarity and fidelity. With a modest "experience base," the Sound Strobe can be a useful tool for that goal. Plus, it's fun to experiment with—you'll hear a very intriguing array of speaker and room (distinguishable) pulse-response sounds that can directly relate to the reproduction of music.

I'd like to thank Ron Tipton (*info@* tdl-tech.com) for his excellent packaging, board layout, and finetuning for production. aX

The Sound Strobe is available in kit or assembled units from Old Colony Sound Lab, PO Box 876, Peterborough, NH 03458, 888-924-9465, e-mail: custserv@audioXpress.com